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# STORMWATER MANAGEMENT CALCULATIONS

# MULTI-STORY MIXED-USE BUILDING

## BLOCK 20403, LOTS 1 & 2

## 682 NJ STATE HIGHWAY ROUTE 440

# **CITY OF JERSEY CITY**

## HUDSON COUNTY, NEW JERSEY

## **PROJECT NO. 20-2206**

Robert L. Costa N.J. Lic. No. 34702 & 4639 Professional Engineer and Planner

> June 6, 2021 Revised September 30, 2021

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**Precipitation Frequency Data Server** 



NOAA Atlas 14, Volume 2, Version 3 Location name: Jersey City, New Jersey, USA\* Latitude: 40.7202°, Longitude: -74.0925° Elevation: 9.38 ft\*\* \* source: ESRI Maps \*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M.Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

### PF\_tabular | PF\_graphical | Maps\_& aerials

### **PF tabular**

| PDS-b    | PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour) <sup>1</sup> |                         |                            |                            |                         |                            |                            |                         | s/hour) <sup>1</sup>    |                     |
|----------|---|-------------------------|----------------------------|----------------------------|-------------------------|----------------------------|----------------------------|-------------------------|-------------------------|---------------------|
| Duration |   |                         |                            | Avera                      | ge recurren             | ce interval (              | years)                     |                         |                         |                     |
|          | 1   | 2                       | 5                          | 10                         | 25                      | 50                         | 100                        | 200                     | 500                     | 1000                |
| 5-min    | <b>4.00</b>   | <b>4.76</b>             | <b>5.65</b>                | <b>6.31</b>                | <b>7.13</b>             | <b>7.70</b>                | 8.30                       | 8.83                    | <b>9.50</b>             | <b>10.0</b>         |
|          | (3.66-4.38)   | (4.37-5.23)             | (5.15-6.20)                | (5.75-6.94)                | (6.46-7.82)             | (6.95-8.46)                | (7.45-9.13)                | (7.87-9.73)             | (8.36-10.5)             | (8.76-11.2)         |
| 10-min   | <b>3.18</b>   | <b>3.79</b>             | <b>4.51</b>                | <b>5.02</b>                | <b>5.65</b>             | <b>6.09</b>                | <b>6.53</b>                | <b>6.92</b>             | <b>7.43</b>             | <b>7.78</b>         |
|          | (2.91-3.49)   | (3.47-4.17)             | (4.11-4.95)                | (4.57-5.51)                | (5.12-6.20)             | (5.50-6.69)                | (5.86-7.18)                | (6.17-7.63)             | (6.53-8.23)             | (6.79-8.65)         |
| 15-min   | <b>2.64</b><br>(2.42-2.89)  | <b>3.17</b> (2.90-3.48) | <b>3.78</b><br>(3.45-4.15) | <b>4.21</b><br>(3.84-4.62) | <b>4.74</b> (4.30-5.21) | <b>5.12</b><br>(4.62-5.63) | <b>5.48</b><br>(4.92-6.02) | <b>5.82</b> (5.18-6.40) | <b>6.22</b> (5.48-6.89) | 6.50<br>(5.67-7.22) |
| 30-min   | <b>1.80</b>   | <b>2.18</b>             | <b>2.67</b>                | <b>3.03</b>                | <b>3.48</b>             | <b>3.82</b>                | <b>4.16</b>                | <b>4.47</b>             | <b>4.89</b>             | <b>5.20</b>         |
|          | (1.65-1.97)   | (1.99-2.39)             | (2.44-2.93)                | (2.76-3.32)                | (3.16-3.83)             | (3.44-4.19)                | (3.73-4.57)                | (3.98-4.93)             | (4.30-5.41)             | (4.53-5.77)         |
| 60-min   | <b>1.12</b>   | <b>1.36</b>             | <b>1.71</b>                | <b>1.96</b>                | <b>2.31</b>             | <b>2.58</b>                | <b>2.85</b>                | <b>3.12</b>             | <b>3.49</b>             | <b>3.77</b>         |
|          | (1.02-1.23)   | (1.25-1.49)             | (1.56-1.87)                | (1.79-2.16)                | (2.10-2.54)             | (2.32-2.83)                | (2.56-3.13)                | (2.78-3.44)             | (3.07-3.86)             | (3.29-4.19)         |
| 2-hr     | 0.688   | 0.838                   | <b>1.06</b>                | <b>1.23</b>                | <b>1.47</b>             | <b>1.67</b>                | <b>1.87</b>                | <b>2.08</b>             | <b>2.37</b>             | <b>2.60</b>         |
|          | (0.628-0.760)   | (0.762-0.925)           | (0.964-1.17)               | (1.12-1.36)                | (1.33-1.62)             | (1.49-1.84)                | (1.66-2.06)                | (1.83-2.29)             | (2.06-2.62)             | (2.24-2.89)         |
| 3-hr     | 0.510   | <b>0.620</b>            | 0.785                      | 0.914                      | <b>1.09</b>             | <b>1.24</b>                | <b>1.39</b>                | <b>1.55</b>             | <b>1.77</b>             | <b>1.95</b>         |
|          | (0.466-0.562)   | (0.566-0.685)           | (0.715-0.867)              | (0.830-1.01)               | (0.987-1.21)            | (1.11-1.37)                | (1.24-1.53)                | (1.37-1.71)             | (1.54-1.96)             | (1.68-2.16)         |
| 6-hr     | <b>0.330</b>  | 0.400                   | <b>0.504</b>               | <b>0.588</b>               | <b>0.706</b>            | 0.805                      | <b>0.909</b>               | <b>1.02</b>             | <b>1.18</b>             | <b>1.31</b>         |
|          | (0.301-0.363)   | (0.366-0.440)           | (0.459-0.553)              | (0.534-0.644)              | (0.637-0.774)           | (0.721-0.882)              | (0.807-0.995)              | (0.897-1.12)            | (1.02-1.30)             | (1.12-1.44)         |
| 12-hr    | <b>0.200</b>  | <b>0.243</b>            | <b>0.308</b>               | <b>0.361</b>               | <b>0.439</b>            | <b>0.505</b>               | <b>0.576</b>               | <b>0.653</b>            | <b>0.766</b>            | 0.860               |
|          | (0.183-0.220)   | (0.222-0.267)           | (0.281-0.337)              | (0.328-0.395)              | (0.396-0.478)           | (0.452-0.550)              | (0.509-0.627)              | (0.571-0.712)           | (0.657·0.836)           | (0.727-0.942)       |
| 24-hr    | <b>0.113</b>  | <b>0.137</b>            | <b>0.175</b>               | <b>0.207</b>               | <b>0.255</b>            | <b>0.297</b>               | <b>0.343</b>               | 0.394                   | 0.469                   | 0.535               |
|          | (0.104-0.123)   | (0.127-0.149)           | (0.161-0.190)              | (0.191-0.225)              | (0.234-0.276)           | (0.270-0.321)              | (0.308-0.370)              | (0.350-0.426)           | (0.411-0.509)           | (0.462-0.582)       |
| 2-day    | 0.066   | <b>0.080</b>            | <b>0.102</b>               | <b>0.120</b>               | <b>0.147</b>            | <b>0.171</b>               | <b>0.196</b>               | <b>0.224</b>            | 0.265                   | 0.300               |
|          | (0.061-0.072)   | (0.073-0.087)           | (0.093-0.111)              | (0.110-0.131)              | (0.134-0.160)           | (0.154-0.186)              | (0.176-0.214)              | (0.199-0.245)           | (0.232-0.291)           | (0.258-0.331)       |
| 3-day    | 0.046   | 0.056                   | <b>0.071</b>               | 0.084                      | <b>0.103</b>            | <b>0.119</b>               | <b>0.136</b>               | 0.155                   | 0.182                   | 0.205               |
|          | (0.043-0.050)   | (0.052-0.061)           | (0.066-0.078)              | (0.077-0.091)              | (0.094-0.112)           | (0.108-0.129)              | (0.122·0.148)              | (0.138-0.169)           | (0.160-0.200)           | (0.178-0.226)       |
| 4-day    | <b>0.037</b>  | 0.044                   | 0.056                      | 0.066                      | 0.081                   | <b>0.093</b>               | <b>0.106</b>               | <b>0.120</b>            | <b>0.141</b>            | <b>0.158</b>        |
|          | (0.034-0.040)   | (0.041-0.048)           | (0.052-0.061)              | (0.061-0.072)              | (0.074-0.087)           | (0.084-0.100)              | (0.096-0.115)              | (0.108-0.131)           | (0.124-0.154)           | (0.138-0.174)       |
| 7-day    | 0.025   | <b>0.029</b>            | 0.037                      | <b>0.043</b>               | <b>0.051</b>            | <b>0.059</b>               | 0.066                      | 0.075                   | 0.087                   | 0.096               |
|          | (0.023-0.026)   | (0.027-0.032)           | (0.034-0.040)              | (0.040-0.046)              | (0.047-0.055)           | (0.054-0.063)              | (0.060-0.072)              | (0.067-0.081)           | (0.077-0.094)           | (0.084-0.105)       |
| 10-day   | 0.019   | 0.023                   | <b>0.029</b>               | <b>0.033</b>               | <b>0.039</b>            | <b>0.044</b>               | 0.050                      | 0.055                   | 0.064                   | 0.070               |
|          | (0.018-0.021)   | (0.022-0.025)           | (0.027-0.031)              | (0.031-0.035)              | (0.036-0.042)           | (0.041-0.048)              | (0.045-0.053)              | (0.050-0.060)           | (0.057-0.069)           | (0.062-0.076)       |
| 20-day   | 0.013   | 0.016                   | 0.019                      | <b>0.021</b>               | <b>0.024</b>            | <b>0.027</b>               | 0.029                      | 0.032                   | 0.035                   | 0.038               |
|          | (0.012-0.014)   | (0.015-0.017)           | (0.017-0.020)              | (0.020-0.022)              | (0.023-0.026)           | (0.025-0.028)              | (0.027-0.031)              | (0.029-0.034)           | (0.032-0.038)           | (0.035-0.041)       |
| 30-day   | <b>0.011</b>  | 0.013                   | 0.015                      | <b>0.017</b>               | 0.019                   | <b>0.021</b>               | 0.022                      | 0.024                   | <b>0.026</b>            | <b>0.028</b>        |
|          | (0.010-0.012)   | (0.012-0.014)           | (0.014-0.016)              | (0.016-0.018)              | (0.018-0.020)           | (0.019-0.022)              | (0.021-0.024)              | (0.022-0.025)           | (0.024-0.028)           | (0.025-0.029)       |
| 45-day   | 0.009   | 0.011                   | 0.013                      | 0.014                      | 0.016                   | 0.017                      | <b>0.018</b>               | <b>0.019</b>            | <b>0.021</b>            | <b>0.022</b>        |
|          | (0.009-0.010)   | (0.010-0.011)           | (0.012-0.013)              | (0.013-0.015)              | (0.015-0.016)           | (0.016-0.018)              | (0.017-0.019)              | (0.018-0.020)           | (0.019-0.022)           | (0.020-0.023)       |
| 60-day   | <b>0.008</b>  | 0.010                   | <b>0.011</b>               | <b>0.012</b>               | <b>0.014</b>            | <b>0.014</b>               | 0.015                      | <b>0.016</b>            | <b>0.017</b>            | 0.018               |
|          | (0.008-0.009)   | (0.009-0.010)           | (0.011-0.012)              | (0.012-0.013)              | (0.013-0.014)           | (0.014-0.015)              | (0.015-0.016)              | (0.015-0.017)           | (0.016-0.018)           | (0.017-0.019)       |

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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### TABLE 7.1

## TYPICAL RUNOFF COEFFICIENTS (C VALUES) FOR 100 YEAR FREQUENCY STORM

### TABLE 7.1

### TYPICAL RUNOFF COEFFICIENTS (C VALUES) FOR 100 YEAR FREQUENCY STORM

|                                  |                        |       | Hydrologic | Soil Group |      |
|----------------------------------|------------------------|-------|------------|------------|------|
| Land Use Description             |                        | A     | <u>B</u>   | Ċ          | D    |
| Cultivated land.                 |                        |       | _          | -          |      |
| without conservation treatme     | ent                    | 0.49  | 0.67       | 0.81       | 0.88 |
| with conservation treatment      |                        | 0.27  | 0.43       | 0.61       | 0.67 |
| Pasture or range land:           |                        |       |            |            |      |
| poor condition                   |                        | 0.38  | 0.63       | 0.78       | 0,84 |
| good condition                   |                        | NA    | 0.25       | 0.51       | 0.65 |
| Meadow: good condition           |                        | NA    | NA         | 0.44       | 0.61 |
| Wood or forest land:             |                        |       |            |            | 0101 |
| thin stand, poor cover, no m     | ulch                   | NA    | NA         | 0.59       | 0.79 |
| good cover                       |                        | NA    | NA         | 0.45       | 0.59 |
| Open spaces, lawns, parks, golf  | courses, cemeteries:   |       |            |            | 0.07 |
| good condition, grass cover of   | on 75% or more of area | NA    | 0.25       | 0.51       | 0.65 |
| fair condition, grass cover on   | 1 50–75% of area       | NA    | 0.45       | 0.63       | 0.74 |
| Commercial and business areas    | s (85% impervious)     | 0.84  | 0.90       | 0.93       | 0.96 |
| Industrial districts (72% imper- |                        | 0.67  | 0.81       | 0.88       | 0.92 |
| Residential:                     |                        |       |            | 0.00       | 0.72 |
| Average lot                      | Average                |       |            |            |      |
| size                             | impervious             |       |            |            |      |
| 1/2 acre                         | 65%                    | 0.59  | 0.76       | 0.86       | 0.90 |
| ∦ acre                           | 38%                    | 0.25  | 0.55       | 0.70       | 0.80 |
| ∦ acre                           | 30%                    | NA    | 0.49       | 0.67       | 0.78 |
| ž acre                           | 25%                    | NA    | 0.45       | 0.65       | 0.76 |
| 1 acre                           | 20%                    | NA    | 0.41       | 0.63       | 0.74 |
| Paved parking lots, roofs, drive |                        | 0.99  | 0.99       | 0.99       | 0.99 |
| Streets and roads:               |                        |       | 077        | 0.00       | 0.99 |
| paved with curbs and storm s     | ewers                  | 0.99  | 0.99       | 0.99       | 0.99 |
| gravel                           |                        | 0.57  | 0.76       | 0.84       | 0.88 |
| dirt                             |                        | 0.49  | 0.69       | 0.80       | 0.84 |
|                                  |                        | Q: 17 | 0.07       | 0.00       | U.64 |

Note:

NA denotes information is not available; design engineers should rely on another authoritative source. New Jersey Department of Environmental Protection, Technical Manual for Land Use Regulation Program, Bureaus of Inland and Coastal Regulations, Stream Encroachment Permits (Trenton, New Jersey: Department of Environmental Protection, Revised September 1995) p. 12. Source:

## Figure 7.1

# TIME OF CONCENTRATION



### Notes:

Use Nomograph  $T_c$  for natural basins with well-defined channels, for overland or bare earth, and for mowed grass roadside channels.

For overland flow, grassed surfaces, multiply  $T_{\rm e}$  by 2.

For overland flow, concrete or asphalt surfaces, multiply  $T_c$  by 0.4.

For concrete channels, multiply  $T_{\rm c}$  by 0.2 overland flow.

Based on a study by P.Z. Kirpich, Civil Engineering, Vol.10, No.6, June 1940, p. 362.



## EXECUTIVE SUMMARY

This project titled "Multi-Story Mixed-Use Building" consists of the new thirteen-story multi-family building consisting of residential dwellings and a parking garage. The project is located in block 20403, lots 1&2 through 19, 682 NJ State Highway Route 404 in the City of Jersey City, Hudson County, New Jersey. Pre-existing conditions and postconditions are shown on the next page.

The Modified Rational Method was used to calculate pre- and postdevelopment peak discharges. Using the required reductions, storage volumes were computed. The 2-year storm produces the greatest storage volume as per the modified rational method. The required storage volume is  $1,223 ft^3$ . To comply with the required storage, this project required 120 LF of 36" ADS pipe with chambers at both ends. The detention system has a capacity of 1,956 cu. ft. with a *circular 6" and 4" orifice* to provide the necessary reductions in the runoff.

This project complies with the new NJDEP Stormwater Management Regulations. Water quantity standards have been addressed by using a 100year storm. Water quality standards have been since all parking areas are located internal to the proposed building. At last, the building will have a green roof to address DEP requirements.

All calculations are made part of this report.

# **Multi-Story Mixed-Use Building**

# 682 NJ State Highway Route 440

# Block 20403, Lots 1& 2

# **City of Jersey City**

# Hudson County, New Jersey

| CI          | EXISTING<br>(CFS)<br>C2 | REDUCTION<br>(CFS)<br>C3 | UN-DETAINED<br>(CFS)<br>C4 | ROUTING<br>(CFS)<br>C5 | ALLOWABLE<br>(CFS)<br>(C3-C4)<br>C6 | STORAGE<br>(CU.FT.)<br>C7 |
|-------------|-------------------------|--------------------------|----------------------------|------------------------|-------------------------------------|---------------------------|
| 2 YEAR      | 2.56                    | 50% = 1.28               | 0.10                       | 1.08                   | 1.18                                | 1,223                     |
| 10<br>YEAR  | 3.39                    | 75% = 2.54               | 0.13                       | 1.59                   | 2.41                                | 836                       |
| 100<br>YEAR | 4.42                    | 80% = 3.54               | 0.16                       | 1.97                   | 3.38                                | 842                       |

## **STORAGE DATA**

| ELEVATION<br>(FT) | OUTFLOW<br>(CFS) | STORAGE<br>(CU.FT.) |
|-------------------|------------------|---------------------|
| 0.00              | 0.00             | 0                   |
| 0.5               | 0.5              | 219                 |
| 1.00              | 0.8              | 575                 |
| 1.50              | 1.1              | 978                 |
| 2.00              | 1.5              | 1,361               |
| 2.50              | 1.8              | 1,722               |
| 3.00              | 2.0              | 1,956               |

## SUMMARY OF PEAK OUTFLOW AND PEAK ELEVATION

|          | PEAK<br>INFLOW<br>(CFS) | PEAK<br>OUTFLOW<br>(CFS) | PEAK<br>ELEVATION<br>(FT) | TOTAL STORAGE<br>IN POND<br>(CU.FT.) |
|----------|-------------------------|--------------------------|---------------------------|--------------------------------------|
| 2 YEAR   | 1.28                    | 1.08                     | 1.47                      | 955                                  |
| 10 YEAR  | 2.44                    | 1.59                     | 2.15                      | 1,472                                |
| 100 YEAR | 3.41                    | 1.97                     | 2.93                      | 1,923                                |

## **PRE-EXISTING:**

| TOTAL:      | 0.683 Acres |
|-------------|-------------|
| IMPERVIOUS: | 0.683 Acres |

### **POST-DEVELOPMENT:**

| PROPOSED AREA | : (UN-DETAINED) |
|---------------|-----------------|
| IMPERVIOUS:   | 0.00154 Acres   |
| GREEN:        | 0.0247 Acres    |

(DETAINED): IMPERVIOUS:

0.66 Acres

### Project Name:- Multi -Story Mixed Use Building Block 20403, Lot 1 & 2 City of Jersey City Hudson County, New Jersey

|   |           | EXISTING<br>CONDITION | REDUCTION | REDUCTION FLOW | UNDETAIN<br>FLOW | ALLOWABLE<br>FLOW | REQUIRED<br>STORAGE |
|---|-----------|-----------------------|-----------|----------------|------------------|-------------------|---------------------|
|   |           | (CFS)                 | (CFS)     | (CFS)          | (CFS)            | (CFS)             | (CU.FT.)            |
| Γ | 2 YEARS   | 2.56                  | 50%       | 1.28           | 0.10             | 1.18              | 1,223               |
|   | 10 YEARS  | 3.39                  | 75%       | 2.54           | 0.13             | 2.41              | 836                 |
|   | 100 YEARS | 4.42                  | 80%       | 3.54           | 0.16             | 3.38              | 842                 |

| Pipe Storage |                  |              |                         |     |                |
|--------------|------------------|--------------|-------------------------|-----|----------------|
| ELEVATION    | D/D <sup>2</sup> | LENGTH (FT.) | D <sup>2</sup> (SQ.FT.) | ROW | TOTAL (CU.FT.) |
| 0.50         | 0.0811           | 120          | 9                       | 2   | 175.18         |
| 1.00         | 0.2260           | 120          | 9                       | 2   | 488.16         |
| 1.50         | 0.3927           | 120          | 9                       | 2   | 848.23         |
| 2.00         | 0.5499           | 120          | 9                       | 2   | 1187.78        |
| 2.50         | 0.6969           | 120          | 9                       | 2   | 1505.30        |
| 3.00         | 0.7854           | 120          | 9                       | 2   | 1696.46        |

| CHAMBER STORAGE |           |       |                |
|-----------------|-----------|-------|----------------|
| ELEVATION       | LENGTH    | WIDTH | NO. OF CHAMBER |
| 0.50            | 10.833333 | 4     | 2              |
| 1.00            | 10.833333 | 4     | 2              |
| 1.50            | 10.833333 | 4     | 2              |
| 2.00            | 10.833333 | 4     | 2              |
| 2.50            | 10.833333 | 4     | 2              |
| 3.00            | 10.833333 | 4     | 2              |

| TOTAL              |  |
|--------------------|--|
| CHAMBER<br>STORAGE |  |
| (CU.FT.)           |  |
| 43.33              |  |
| 86.67              |  |
| 130.00             |  |
| 173.33             |  |
| 216.67             |  |
| 260.00             |  |

## TOTAL STORAGE

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| PIPE    | CHAMBER   | TOTAL STORAGE   |
|---------|---|---|
| STORAGE | STORAGE   | (Cu.FT.)  |
| 175.18  | 43.33   | 219   |
| 488.16  | 86.67   | 575   |
| 848.23  | 130.00  | 978   |
| 1187.78 | 173.33  | 1361  |
| 1505.30 | 216.67  | 1722  |
| 1696.46 | 260.00  | 1956  |
|         | STORAGE<br>175.18<br>488.16<br>848.23<br>1187.78<br>1505.30 | STORAGE         STORAGE           175.18         43.33           488.16         86.67           848.23         130.00           1187.78         173.33           1505.30         216.67 |



Quick TR-55 Ver.5.46 S/N: Executed: 13:10:20 06-15-2021

> PRE DEVELOPMENT ANALYSIS FOR THE 2 YEAR STORM MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ

\* \* \* \* \* SUMMARY OF RATIONAL METHOD PEAK DISCHARGES \* \* \* \* \* \*

Q = adj \* C \* I \* A

Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

|                   |               |               |             | RETURN FREQUENCY = 2 years<br>`C' adjustment, k = 1<br>Adj. 'C' = Wtd.'C' x 1 |     |             |            |                |                 |  |  |  |
|-------------------|---------------|---------------|-------------|---|-----|-------------|------------|----------------|-----------------|--|--|--|
|                   |               |               |             |   | = : |             | =========  | ========       | =======         |  |  |  |
| Subarea<br>Descr. | Runoff<br>'C' | Area<br>acres | TC<br>(min) | Wtd.<br>'C'   |     | Adj.<br>'C' | I<br>in/hr | Total<br>acres | Peak Q<br>(cfs) |  |  |  |
| IMPERVIOUS        | 0.990         | 0.68          |             |   |     |             |            |                |                 |  |  |  |
|                   |               |               | 10.00       | 0.990   | ŀ   | 0.990       | 3.790      | 0.68           | 2.56            |  |  |  |

Ouick TR-55 Ver.5.46 S/N: Executed: 13:11:33 06-15-2021 PRE DEVELOPMENT ANALYSIS FOR THE 10 YEAR STORM MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ \* \* \* \* \* SUMMARY OF RATIONAL METHOD PEAK DISCHARGES \* \* \* \* \* \* Q = adj \* C \* I \* AWhere: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency RETURN FREQUENCY = 10 years `C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1 SubareaRunoffAreaTcWtd.Descr.'C'acres(min)'C' Adj. I Total 'C' in/hr acres Subarea Runoff Area Wtd. Peak Q (cfs) -----IMPERVIOUS 0.990 0.68 10.00 0.990 0.990 5.020 0.68 3.39 Quick TR-55 Ver.5.46 S/N: Executed: 13:12:41 06-15-2021

> PRE DEVELOPMENT ANALYSIS FOR THE 100 YEAR STORM MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ

\* \* \* \* \* SUMMARY OF RATIONAL METHOD PEAK DISCHARGES \* \* \* \* \* \*

Q = adj \* C \* I \* A

Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

|                   |               |               |             |             |     | `C' adj     | ustment,   | ICY = 100<br>k = 1<br>l.'C' x 1  | years           |
|-------------------|---------------|---------------|-------------|-------------|-----|-------------|------------|----------------------------------|-----------------|
|                   |               |               |             |             | = : |             | =========  | ========                         | ========        |
| Subarea<br>Descr. | Runoff<br>'C' | Area<br>acres | Tc<br>(min) | Wtd.<br>'C' |     | Adj.<br>'C' | I<br>in/hr | Total<br>acres                   | Peak Q<br>(cfs) |
| IMPERVIOUS        | 0.990         | 0.68          |             |             |     |             |            | - dhe odd war kan kar on war air |                 |
|                   |               |               | 10.00       | 0.990       |     | 0.990       | 6.530      | 0.68                             | 4.42            |

Quick TR-55 Ver.5.46 S/N: Executed: 13:39:25 06-15-2021 POST DEVELOPMENT ANALYSIS FOR THE 2 YEAR STORM (UNDETAIN AREA) MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ \* \* \* \* \* SUMMARY OF RATIONAL METHOD PEAK DISCHARGES \* \* \* \* \* \* Q = adj \* C \* I \* AWhere: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency RETURN FREQUENCY = 2 years C' adjustment, k = 1 Adj.  $'C' = Wtd. 'C' \times 1$ SubareaRunoffAreaTcWtd.Adj.ITotalPeak QDescr.'C'acres(min)'C''C'in/hracres(cfs) IMPERVIOUS 0.990 0.00 GREEN 0.960 0.02 10.00 0.962 0.962 3.790 0.03 0.10 Quick TR-55 Ver.5.46 S/N: Executed: 13:43:11 06-15-2021 POST DEVELOPMENT ANALYSIS FOR THE 10 YEAR STORM (UNDETAIN AREA) MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ \* \* \* \* \* SUMMARY OF RATIONAL METHOD PEAK DISCHARGES \* \* \* \* \* \* Q = adj \* C \* I \* AWhere: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency **RETURN FREQUENCY = 10** years C' adjustment, k = 1Adj.  $C' = Wtd. C' \times 1$ Adj. I Total 'C' in/hr acres TC Wtd. (min) 'C' Subarea Runoff Area Peak Q Descr. 'C' acres (cfs) \_\_\_\_ IMPERVIOUS0.9900.00GREE0.9600.02 10.00 0.962 0.962 5.020 0.03 0.13 Quick TR-55 Ver.5.46 S/N: Executed: 13:44:43 06-15-2021 POST DEVELOPMENT ANALYSIS FOR THE 100 YEAR STORM (UNDETAIN AREA) MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ \* \* \* \* \* SUMMARY OF RATIONAL METHOD PEAK DISCHARGES \* \* \* \* \* \* Q = adj \* C \* I \* AWhere: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency **RETURN FREQUENCY** = 100 years C' adjustment, k = 1Adj.  $'C' = Wtd. 'C' \times 1$ \_\_\_\_\_ Adj. I Total 'C' in/hr acres Peak Q Subarea Runoff Area TC Wtd. (min) 'C' Descr. 'C' acres (cfs) \_\_\_\_\_ \_\_\_\_\_ IMPERVIOUS0.9900.00GREEN0.9600.02 10.00 0.962 0.962 6.530 0.03 0.16



MODIFIED RATIONAL METHOD ---- Graphical Summary for Maximum Required Storage ----

First peak outflow point assumed to occur at inflow recession leg.

POST DEVELOPMENT ANALYSIS FOR THE 2 YEAR STORM MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ



LOW Cfs

F

> MODIFIED RATIONAL METHOD ---- Summary for Single Storm Frequency ----

First peak outflow point assumed to occur at inflow recession leg.

POST DEVELOPMENT ANALYSIS FOR THE 2 YEAR STORM MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ

| RETURN FR                        | EQUENCY:                                | 2 yr 🗋                                  | C' Adjust                       | ment = 1 | .000 All | owable Q =                 | 1.18 cfs |
|----------------------------------|---|---|---------------------------------|----------|----------|----------------------------|----------|
|                                  |   |   |                                 |          |          |                            |          |
|                                  | h file dur                              |   |                                 | tes      |          |                            |          |
|                                  | h file: 20                              |   |                                 |          |          | TC = 10.00                 |          |
| * * * * * * * * * * * *          | • • • • • • • • • • • • • • • • • • •   | · · · · · · · · · · ·                   | * * * * * * * * * * *           |          |          | VOLU                       |          |
| Weighted                         | Adjusted                                | Duration                                |                                 | Areas    | Qpeak    | Inflow                     | <b>~</b> |
| `C'                              | īĊŗ                                     | minutes                                 | in/hr                           | acres    | cfs      | (cu.ft.)                   | (cu.ft.) |
| 0.990                            | 0.990                                   | 10                                      | 3.790                           | 0.66     | 2.48     | 1,486                      | 778      |
|                                  |   | 15                                      | 3.170                           | 0.66     | 2.07     | 1,864                      |          |
|                                  |   | 20                                      |                                 | 0.66     | 1.86     | 2,227                      |          |
| 0.990                            | 0.990                                   | 30                                      | 2.180                           | 0.66     | 1.42     | 2,564                      | 1,148    |
| ula ala ala ala ala ala da da da | a alar alar alar alar alar alar alar al | - ala ala ala ala ala ala ala ala ala a | ىلە بۇرىلە بۇرىلە بۇرىلە بۇرىلە | ***      |          | ***** Storag               |          |
| 0.990                            |   |   |                                 |          |          | 2,922                      |          |
|                                  |   |   |                                 | *******  | ⊥        | <i>L; JLL</i><br>********* |          |
|                                  |   |   |                                 |          |          |                            |          |
| 0.990                            | 0.990                                   | 40                                      | 1.907                           | 0.66     | 1.25     | 2,990                      | 1,220    |
| 0.990                            | 0.990                                   | 50                                      | 1.633                           | 0.66     | 1.07     | Qpeak <                    | Qallow   |

| ******    | *******    | ******    | *******   | ******        | **********   | ************ | * * * * * * * |
|-----------|------------|-----------|-----------|---------------|--------------|--------------|---------------|
| *****     | *****      | *******   | ******    | ******        | ****         | *****        | *****         |
| *         |            |           |           |               |              |              | *             |
| *         |            |           |           |               |              |              | *             |
| *         |            | 3.6       |           | DAMITONIA     |              |              | *             |
|           |            |           |           |               | L METHOD     | ·            |               |
| *         | G          | rand Summ | ary For   | ALL STO       | rm Frequenc: | Les          | *             |
| *         |            |           |           |               |              |              | *             |
| *         |            |           |           |               |              |              | *             |
| ******    | ******     | *******   | ******    | ******        | ********     | ***********  | ******        |
| ******    | ******     | *******   | ******    | ******        | *****        | ***********  | *****         |
|           |            |           |           |               |              |              |               |
| Fire      | t neak out | flow poin | t aggume  | d to oc       | cur at inflo | w recession  | lea           |
| 1.47.0    | c peak out | rrow born | c appulle | u 10 00       |              |              | Leg.          |
|           |            |           |           | TO BOD        |              |              |               |
|           |            |           |           |               | THE 2 YEAD   |              |               |
|           |            |           |           | •             | L 20403, LO  |              |               |
| 1         | 682        | NJ STATE  | HIGHWAY   | RT 440,       | JERSEY CITY  | (, NJ        |               |
|           |            |           |           |               |              |              |               |
|           | A          | rea =     | 0.66 ac   | res           |              | TC = 10.00   | minutes       |
|           |            |           |           | : : : : : : : |              |              |               |
|           |            |           |           |               |              | VOLU         | MES           |
| Frequency | Adjusted   | Duration  | Intens    | Opeak         | Allowable    | Inflow       |               |
|           | 'C'        |           |           |               |              | (cu.ft.)     |               |
| (Years)   |            | minures   | 111/111   | CID           | CT0          | (cu.rc.)     | (Cu.IC.)      |
| <u></u>   | 0 000      | 20        | 1 0/1     | 1 20          | 1 10         | 2 022        | 1 222         |
| 2         | 0.990      | 38        | T.20T     | 1.28          | 1.18         | 2,922        | 1,223         |

> POST DEVELOPMENT ANALYSIS FOR THE 2 YEAR STORM MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ

\* \* \* \* \* SUMMARY OF RATIONAL METHOD PEAK DISCHARGES \* \* \* \* \* \*

Q = adj \* C \* I \* A Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

|            |        |       |       |       |    | `C' adj            | ustment, | CY = 2<br>k = 1<br>.'C' x 1 | years  |
|------------|--------|-------|-------|-------|----|--------------------|----------|-----------------------------|--------|
| Subarea    | Runoff | Area  | Тс    | Wtd.  | =: | ========<br>  Adj. | <br>T    | Total                       | Peak Q |
| Descr.     | 'C'    | acres | (min) | 'C'   |    | 'C'                | in/hr    | acres                       | (cfs)  |
| IMPERVIOUS | 0.990  | 0.66  |       |       |    |                    |          |                             |        |
|            |        |       | 10.00 | 0.990 |    | 0.990              | 3.790    | 0.66                        | 2.48   |

Quick TR-55 Ver.5.46 S/N: Executed: 09:58:17 09-30-2021 POST DEVELOPMENT ANALYSIS FOR THE 2 YEAR STORM MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ \*\*\*\* Modified Rational Hydrograph \*\*\*\*\* Weighted C = 0.990 Area = 0.660 acres Tc = 10.00 minutes Adjusted C = 0.990 Td= 38.00 min. I= 1.96 in/hr Qp= 1.28 cfs **RETURN FREQUENCY:** 2 year storm Adj.factor = 1.00 Output file: 2022A2 .HYD HYDROGRAPH FOR MAXIMUM STORAGE For the 2 Year Storm Time Time increment = 0.017 Hours Time on left represents time for first Q in each row. Hours 

| 0.000 | 0.00 | 0.13 | 0.26 | 0.38 | 0.51 | 0.64 | 0.77 |
|-------|------|------|------|------|------|------|------|
| 0.117 | 0.90 | 1.03 | 1.15 | 1.28 | 1.28 | 1.28 | 1.28 |
| 0.233 | 1.28 | 1.28 | 1.28 | 1.28 | 1.28 | 1.28 | 1.28 |
| 0.350 | 1.28 | 1.28 | 1.28 | 1.28 | 1.28 | 1.28 | 1.28 |
| 0.467 | 1.28 | 1.28 | 1.28 | 1.28 | 1.28 | 1.28 | 1.28 |
| 0.583 | 1.28 | 1.28 | 1.28 | 1.28 | 1.15 | 1.03 | 0.90 |
| 0.700 | 0.77 | 0.64 | 0.51 | 0.38 | 0.26 | 0.13 | 0.00 |

### MODIFIED RATIONAL METHOD ---- Graphical Summary for Maximum Required Storage ----

First peak outflow point assumed to occur at inflow recession leg.

POST DEVELOPMENT ANALYSIS FOR THE 10 YEAR STORM MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ

Allowable Outflow: RETURN FREQUENCY: 10 yr 2.41 cfs \* 'C' Adjustment: 1.000 Required Storage: 836 cu.ft. \* \* \_\_\_\_\_ . \_ \* \*\_\_\_\_\_ \* Inflow .HYD stored: 2022A10 .HYD Peak Inflow: 2.44 cfs 



Executed: 10:08:27 09-30-2021 POST DEVELOPMENT ANALYSIS FOR THE 10 YEAR STORM MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ \*\*\*\* Modified Rational Hydrograph \*\*\*\*\* Weighted C = 0.990 Area = 0.660 acres Tc = 10.00 minutes Adjusted C = 0.990 Td= 21.00 min. I= 3.74 in/hr Qp= 2.44 cfs RETURN FREQUENCY: 10 year storm Adj.factor = 1.00 Output file: 2022A10 .HYD HYDROGRAPH FOR MAXIMUM STORAGE For the 10 Year Storm Time increment = 0.017 Hours Time Time on left represents time for first Q in each row. Hours 

Quick TR-55 Ver.5.46 S/N:

| 0.000 | 0.00 | 0.24 | 0.49 | 0.73 | 0.98 | 1.22 | 1.47 |
|-------|------|------|------|------|------|------|------|
| 0.117 | 1.71 | 1.95 | 2.20 | 2.44 | 2.44 | 2.44 | 2.44 |
| 0.233 | 2.44 | 2.44 | 2.44 | 2.44 | 2.44 | 2.44 | 2.44 |
| 0.350 | 2.44 | 2.20 | 1.95 | 1.71 | 1.47 | 1.22 | 0.98 |
| 0.467 | 0.73 | 0.49 | 0.24 | 0.00 |      |      |      |

> POST DEVELOPMENT ANALYSIS FOR THE 10 YEAR STORM MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ

\* \* \* \* \* SUMMARY OF RATIONAL METHOD PEAK DISCHARGES \* \* \* \* \* \*

Q = adj \* C \* I \* A

Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

|                   |               |               |             |             |     | `C' adj     | FREQUEN<br>ustment,<br>C' = Wtd |                | years           |
|-------------------|---------------|---------------|-------------|-------------|-----|-------------|---------------------------------|----------------|-----------------|
|                   |               |               |             |             | = = |             | =========                       | =========      | ========        |
| Subarea<br>Descr. | Runoff<br>'C' | Area<br>acres | TC<br>(min) | Wtd.<br>'C' |     | Adj.<br>'C' | I<br>in/hr                      | Total<br>acres | Peak Q<br>(cfs) |
| IMPERVIOUS        | 0.990         | 0.66          |             |             |     |             |                                 |                |                 |
|                   |               |               | 10.00       | 0.990       |     | 0.990       | 5.020                           | 0.66           | 3.28            |

| *****                | ******                  | ********            | *******  | ******  | **********                               | **********         | ******           |
|----------------------|-------------------------|---------------------|----------|---------|--|--------------------|------------------|
| *****                | *****                   | ******              | ******   | ******  | *****                                    | ******             | ******           |
| *                    |                         |                     |          |         |  |                    | *                |
| *                    |                         |                     |          |         |  |                    | *                |
| *                    |                         | 344                 |          |         |  |                    |                  |
|                      | ~                       |                     |          |         | L METHOD                                 | ·                  | -h               |
| *                    | G                       | rand Summa          | ary For  | All Sto | rm Frequenc:                             | les                | *                |
| *                    |                         |                     |          |         |  |                    | *                |
| *                    |                         |                     |          |         |  |                    | *                |
| ******               | ******                  | *******             | ******   | ******  | *******                                  | ******             | ******           |
| ******               | ******                  | *******             | ******   | ******  | ******                                   | *****              | ******           |
|                      | MULTI                   | STORY MIXI          | ED USE B | LDG., B | THE 10 YEAD<br>L 20403, LO<br>JERSEY CIT | Г1&2               | -                |
|                      | А                       | rea =               | 0.66 ac  | res     |  | Tc = 10.00         | minutes          |
|                      | * * * * * * * * * * * * |                     |          | ::::::  | * * * * * * * * * * * * * *              | VOLU               | :::::::::<br>MES |
| Frequency<br>(years) |                         | Duration<br>minutes |          |         |  | Inflow<br>(cu.ft.) |                  |
| 10                   | 0.990                   | 21                  | 3.738    | 2.44    | 2.41                                     | 3,077              | 836              |

> MODIFIED RATIONAL METHOD ---- Summary for Single Storm Frequency ----

First peak outflow point assumed to occur at inflow recession leg.

POST DEVELOPMENT ANALYSIS FOR THE 10 YEAR STORM MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ

| RETURN FR       | EQUENCY:                              | 10 yr `C            | ' Adjust | ment = 1.            | 000 All              | owable Q =                           | 2.41 cfs |
|-----------------|---------------------------------------|---------------------|----------|----------------------|----------------------|--------------------------------------|----------|
|                 | h file dur<br>h file: 20<br>::::::::: |                     |          |                      |                      | TC = 10.00<br>:::::::::::<br>VOLU    |          |
| Weighted<br>`C' | Adjusted<br>'C'                       | Duration<br>minutes |          | Areas<br>acres       | Qpeak<br>cfs         | Inflow<br>(cu.ft.)                   |          |
| 0.990           | +                                     | 10<br>15<br>20      |          | 0.66<br>0.66<br>0.66 | 3.28<br>2.75<br>2.49 | 1,968 <sup>.</sup><br>2,476<br>2,993 |          |
|                 | 0.990                                 |                     | 3.738    |                      |                      | ***** Storage<br>3,077               |          |
| 0.990           |                                       |                     |          | 0.66                 | 1.98                 | Qpeak <                              | Qallow   |

### MODIFIED RATIONAL METHOD ---- Graphical Summary for Maximum Required Storage

First peak outflow point assumed to occur at inflow recession leg.

POST DEVELOPMENT ANALYSIS FOR THE 100 YEAR STORM MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ



> POST DEVELOPMENT ANALYSIS FOR THE 100 YEAR STORM MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ

\*\*\*\* Modified Rational Hydrograph \*\*\*\*\* Weighted C = 0.990 Area = 0.660 acres Tc = 10.00 minutes

Adjusted C = 0.990 Td= 18.00 min. I= 5.22 in/hr Qp= 3.41 cfs

RETURN FREQUENCY: 100 year storm Adj.factor = 1.00 Output file: 2022A100.HYD

> HYDROGRAPH FOR MAXIMUM STORAGE For the 100 Year Storm

| Time<br>Hours                             | Time                                 |                              | ime increme<br>represents    |                              |                              | in each r                    | ω.                           |
|---|--------------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 0.000<br>0.117<br>0.233<br>0.350<br>0.467 | 0.00<br>2.39<br>3.41<br>2.39<br>0.00 | 0.34<br>2.73<br>3.41<br>2.04 | 0.68<br>3.07<br>3.41<br>1.70 | 1.02<br>3.41<br>3.41<br>1.36 | 1.36<br>3.41<br>3.41<br>1.02 | 1.70<br>3.41<br>3.07<br>0.68 | 2.04<br>3.41<br>2.73<br>0.34 |

> POST DEVELOPMENT ANALYSIS FOR THE 100 YEAR STORM MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ

\* \* \* \* \* SUMMARY OF RATIONAL METHOD PEAK DISCHARGES \* \* \* \* \* \*

Q = adj \* C \* I \* A

Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

|                   |               |               | RETURN FREQUENCY = 100<br>`C' adjustment, k = 1<br>Adj. 'C' = Wtd.'C' x 1 |             |    |             |            | years          |                 |
|-------------------|---------------|---------------|---|-------------|----|-------------|------------|----------------|-----------------|
|                   |               |               |   |             | == |             |            | ========       |                 |
| Subarea<br>Descr. | Runoff<br>'C' | Area<br>acres | TC<br>(min)   | Wtd.<br>'C' |    | Adj.<br>'C' | I<br>in/hr | Total<br>acres | Peak Q<br>(cfs) |
| IMPERVIOUS        | 0.990         | 0.66          |   |             |    |             |            |                |                 |
|                   |               |               | 10.00   | 0.990       |    | 0.990       | 6.530      | 0.66           | 4.27            |

\* \* \* \* MODIFIED RATIONAL METHOD  $\mathbf{\star}$ \* \* ---- Grand Summary For All Storm Frequencies ----\* \* \* +First peak outflow point assumed to occur at inflow recession leg. POST DEVELOPMENT ANALYSIS FOR THE 100 YEAR STORM MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ Area = 0.66 acres Tc = 10.00 minutesVOLUMES Frequency Adjusted Duration Intens. Qpeak. Allowable Inflow Storage (years) 'C' minutes in/hr cfs cfs (cu.ft.) (cu.ft.) 100 0.990 18 5.216 3.41<sup>,</sup> 3.38 3,681 842

MODIFIED RATIONAL METHOD

First peak outflow point assumed to occur at inflow recession leg.

POST DEVELOPMENT ANALYSIS FOR THE 100 YEAR STORM MULTI STORY MIXED USE BLDG., BL 20403, LOT 1 & 2 682 NJ STATE HIGHWAY RT 440, JERSEY CITY, NJ

| RETURN FR  | EQUENCY: 1 | .00 yr `C | C' Adjust | ment = 1 | .000 All | owable Q =      | 3.38 cfs |
|--|------------|-----------|-----------|----------|----------|-----------------|----------|
|  |            |           |           |          |          |                 |          |
|  | h file dur |           |           | ites     |          | $T_{2} = 10.00$ | minutoq  |
| Hydrograph file: 2022A100.HYD Tc = 10.00 minutes |            |           |           |          |          |                 |          |
|  |            |           |           |          |          | VOLU            | MES      |
| Weighted   | Adjusted   |           |           | Areas    | Qpeak    | Inflow          | Storage. |
| `Č'  | 'C'        | minutes   | in/hr     | acres    | cfs      | (cu.ft.)        | (cu.ft.) |
| 0.990  | 0.990      | 10        | 6.530     | 0.66     | 4.27     | 2,560           | 532      |
| 0.990.   | 0.990      | 15        | 5.480     | 0.66     | 3.58     | 3,223           | 688      |
| **************************************           |            |           |           |          |          |                 |          |
| 0.990  | 0.990      | 18        | 5.216     | 0.66     |          |                 |          |
| ******   | *****      | *******   | *******   | *****    | ******   | *******         | *****    |
| 0.990  | 0.990      | 20        | 5.040     | 0.66     | 3.29     | Qpeak <         | Qallow   |



| Outlet Structure File:                 | 2021 .STR              |   |
|--|------------------------|---|
| POND-2 Version: 5.21<br>Date Executed: | S/N:<br>Time Executed: |   |
| ********                               | ******                 | * |

OUTLET STRUCTURE FOR 682 NJ STATE HIGHWAY ROUTE 440 BLOCK 20403, LOT 1 & 2 CITY OF JERSEY CITY, HUDSON COUNTY, NJ

#### \*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*

| Elevation (ft) | Q (cfs) | Contributing Structures |
|----------------|---------|-------------------------|
|                |         |                         |
| 0.00           | 0.0     |                         |
| 0.50           | 0.5     | 1                       |
| 1.00           | 0.8     | 1                       |
| 1.50           | 1.1     | 1                       |
| 2.00           | 1.5     | 2 +1                    |
| 2.50           | 1.8     | 2 +1                    |
| 3.00           | 2.0     | 2 +1                    |
Outlet Structure File: 2021 .STR POND-2 Version: 5.21 S/N: Date Executed: Time Executed: OUTLET STRUCTURE FOR 682 NJ STATE HIGHWAY ROUTE 440 BLOCK 20403, LOT 1 & 2 CITY OF JERSEY CITY, HUDSON COUNTY, NJ Outlet Structure File: C:\PONDPACK\2021 .STR Planimeter Input File: \*\*\* NONE \*\*\* Rating Table Output File: C:\PONDPACK\2021 .PND Min. Elev. (ft) = 0 Max. Elev. (ft) = 3 Incr. (ft) = .5Additional elevations (ft) to be included in table: \* SYSTEM CONNECTIVITY StructureNo.Q TableQ TableORIFICE2->2ORIFICE1->1

Outflow rating table summary was stored in file: C:\PONDPACK\2021 .PND Outlet Structure File: 2021.STRPOND-2 Version: 5.21S/N:Date Executed:Time Executed:

>>>>> Structure No. 2 <<<<< (Input Data)

ORIFICE Orifice - Based on Area and Datum Elevation

E1 elev.(ft)?1.7266E2 elev.(ft)?3.001Orifice coeff.?0.6Invert elev.(ft)?1.56Datum elev.(ft) ?1.7266Orifice area (sq ft)?0.087266

OUTLET STRUCTURE FOR 682 NJ STATE HIGHWAY ROUTE 440 BLOCK 20403, LOT 1 & 2 CITY OF JERSEY CITY, HUDSON COUNTY, NJ

>>>>> Structure No. 1 <<<<< (Input Data)

ORIFICE Orifice - Based on Area and Datum Elevation

E1 elev.(ft)? 0.25 E2 elev.(ft)? 3.001 Orifice coeff.? 0.6 Invert elev.(ft)? 0 Datum elev.(ft) ? 0.25 Orifice area (sq ft)? 0.19635

| Outlet Structure Fil                                      | le: 2021                    | . STR   |
|---|-----------------------------|---|
| POND-2 Version: 5.23<br>Date Executed:                    | L                           | S/N:<br>Time Executed:  |
| BLC<br>CITY OF JER  | CK 20403, L<br>RSEY CITY, H | IUDSON COUNTY, NJ   |
| ************  | *********                   | ******  |
| Outflow Rating Table<br>ORIFICE Orifice                   |                             | ure #2<br>Area and Datum Elevation  |
| Elevation (ft) Q  |                             | mputation Messages  |
| 0.50<br>1.00<br>1.50<br>2.00<br>2.50                      | 0.0 E<br>0.0 E<br>0.0 E     | <pre>2 &lt; E1=1.7266<br/>3 &lt; E1=1.7266<br/>4 &lt; E1=1.7266<br/>5 &lt; E1=1.7266<br/>5 &lt; E1=1.7266<br/>5 = .273<br/>5 = .773</pre> |
| C = .6 A = .087<br>H (ft) = Table el<br>Q (cfs) = C * A * | lev Datum                   | n elev. ( 1.7266 ft )   |

| FOR 682 1<br>LOCK 2040   | **************************************                          |
|--------------------------|---|
| *****                    | *******   |
| Q (cfs)                  | Computation Messages  |
|                          |   |
|                          | E < E1 = 0.25   |
| 0.5                      | E < E1=0.25<br>H =.25<br>H =.750                                |
| 0.5<br>0.8<br>1.1        | H = .25<br>H = .750<br>H = 1.25                                 |
| 0.5<br>0.8<br>1.1<br>1.3 | H = .25<br>H = .750   |
|                          | LOCK 2040:<br>BRSEY CIT<br>*********<br>le for Str<br>e - Based |



POND-2 Version: 5.21 S/N: Page 1 EXECUTED: 09-30-2021 10:19:00  $\mathbf{+}$  $\pm$ \* OUTLET STRUCTURE FOR 682 NJ STATE HIGHWAY ROUTE 440  $\star$ BLOCK 20403, LOT 1 & 2 \* \* \* CITY OF JERSEY CITY, HUDSON COUNTY, NJ \* \* \* \* Inflow Hydrograph: C:\PONDPACK\2022A2 .HYD Rating Table file: C:\PONDPACK\2021 .PND ----INITIAL CONDITIONS----Elevation = 0.00 ft Outflow = 0.00 cfs Storage = 0 cu-0 cu-ft

## GIVEN POND DATA

| ELEVATION | OUTFLOW | STORAGE |
|-----------|---------|---------|
| (ft)      | (cfs)   | (cu-ft) |
|           |         |         |
| 0.00      | 0.0     | 0       |
| 0.50      | 0.5     | 219     |
| 1.00      | 0.8     | 575     |
| 1.50      | 1.1     | 978     |
| 2.00      | 1.5     | 1,361   |
| 2.50      | 1.8     | 1,722   |
| 3.00      | 2.0     | 1,956   |
|           |         |         |

### INTERMEDIATE ROUTING COMPUTATIONS

| 2S/t  | 2S/t + 0 |
|-------|----------|
| (cfs) | (cfs)    |
| 0.0   | 0.0      |
| 7.3   | 7.8      |
| 19.2  | 20.0     |
| 32.6  | 33.7     |
| 45.4  | 46.9     |
| 57.4  | 59.2     |
| 65.2  | 67.2     |

Time increment (t) = 0.017 hrs.

## POND-2 Version: 5.21 S/N: EXECUTED: 09-30-2021 10:19:00

| Pond File:          | C:\PONDPACK\2021   | . PND |
|---------------------|--------------------|-------|
| Inflow Hydrograph:  | C:\PONDPACK\2022A2 | .HYD  |
| Outflow Hydrograph: | C:\PONDPACK\OUT    | . HYD |

## INFLOW HYDROGRAPH

## ROUTING COMPUTATIONS

| · · ·  | FLOW  | I1+I2  | 2S/t - 0  | 2S/t + 0  | OUTFLOW   | ELEVATION  |
|--|---|--|---|---|---|--|
|  | fs)   | (cfs)  | (cfs)   | (cfs)   | (cfs)   | (ft)   |
| $ \begin{array}{c} (hrs) & (c\\ \hline & \\ 0.000 \\ 0.017 \\ 0.033 \\ 0.050 \\ 0.067 \\ 0.083 \\ 0.100 \\ 0.117 \\ 0.133 \\ 0.150 \\ 0.167 \\ 0.183 \\ 0.200 \\ 0.217 \\ 0.233 \\ 0.250 \\ 0.267 \\ 0.283 \\ 0.200 \\ 0.267 \\ 0.283 \\ 0.300 \\ 0.317 \\ 0.333 \\ 0.350 \\ 0.367 \\ 0.383 \\ 0.400 \\ 0.317 \\ 0.333 \\ 0.350 \\ 0.367 \\ 0.383 \\ 0.400 \\ 0.417 \\ 0.433 \\ 0.450 \\ 0.467 \\ 0.483 \\ 0.500 \\ 0.517 \\ 0.533 \\ 0.550 \\ 0.567 \\ 0.583 \\ 0.600 \\ 0.617 \\ 0.633 \\ 0.650 \\ 0.667 \end{array} $ | fs)<br><br>0.00<br>0.13<br>0.26<br>0.38<br>0.51<br>0.64<br>0.77<br>0.90<br>1.03<br>1.15<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28<br>1.28 | $\begin{array}{c} 0.1\\ 0.4\\ 0.6\\ 0.9\\ 1.2\\ 1.4\\ 1.7\\ 1.9\\ 2.2\\ 2.4\\ 2.6\\ 2.6\\ 2.6\\ 2.6\\ 2.6\\ 2.6\\ 2.6\\ 2.6$ | (cfs)<br>0.0<br>0.1<br>0.4<br>0.9<br>1.6<br>2.4<br>3.3<br>4.3<br>5.5<br>6.7<br>8.0<br>9.5<br>10.8<br>12.1<br>13.3<br>14.5<br>15.6<br>16.6<br>17.6<br>18.6<br>19.5<br>20.4<br>21.2<br>22.0<br>22.7<br>23.5<br>24.2<br>24.8<br>25.5<br>26.1<br>26.7<br>27.2<br>27.7<br>28.2<br>29.6<br>30.1<br>30.5<br>30.7<br>30.8 | $\begin{array}{c} 0.0\\ 0.1\\ 0.5\\ 1.1\\ 1.8\\ 2.7\\ 3.8\\ 5.0\\ 6.3\\ 7.7\\ 9.1\\ 10.6\\ 12.0\\ 13.4\\ 14.7\\ 15.9\\ 17.0\\ 13.4\\ 14.7\\ 15.9\\ 17.0\\ 18.1\\ 19.2\\ 20.2\\ 21.1\\ 22.1\\ 22.2\\ 21.1\\ 22.9\\ 23.7\\ 24.5\\ 25.3\\ 26.0\\ 26.7\\ 27.4\\ 28.0\\ 28.6\\ 29.2\\ 29.8\\ 30.3\\ 31.8\\ 32.2\\ 32.6\\ 32.9$ | (cfs)<br>0.00<br>0.01<br>0.03<br>0.07<br>0.12<br>0.18<br>0.24<br>0.32<br>0.40<br>0.49<br>0.53<br>0.57<br>0.60<br>0.64<br>0.67<br>0.70<br>0.73<br>0.76<br>0.73<br>0.76<br>0.78<br>0.81<br>0.83<br>0.85<br>0.86<br>0.88<br>0.90<br>0.92<br>0.93<br>0.95<br>0.96<br>0.98<br>0.99<br>1.00<br>1.01<br>1.03<br>1.04<br>1.05<br>1.06<br>1.07<br>1.08<br>1.08<br>1.08 | (ft)<br>0.00<br>0.01<br>0.03<br>0.07<br>0.12<br>0.18<br>0.24<br>0.32<br>0.40<br>0.49<br>0.55<br>0.61<br>0.67<br>0.73<br>0.73<br>0.78<br>0.83<br>0.83<br>0.88<br>0.93<br>0.97<br>1.01<br>1.04<br>1.04<br>1.04<br>1.04<br>1.08<br>1.11<br>1.14<br>1.17<br>1.22<br>1.25<br>1.27<br>1.29<br>1.32<br>1.34<br>1.36<br>1.38<br>1.40<br>1.41<br>1.43<br>1.45<br>1.47<br>1.47 |
| 0.683  | 0.90  | 1.9  | 30.5  | 32.7  | 1.08  | 1.46   |
| 0.700  | 0.77  | 1.7  | 30.1  | 32.2  | 1.07  | 1.45   |
| 0.717  | 0.64  | 1.4  | 29.4  | 31.5  | 1.05  | 1.42   |
| 0.733  | 0.51  | 1.2  | 28.5  | 30.5  | 1.03  | 1.38   |

## POND-2 Version: 5.21 S/N: EXECUTED: 09-30-2021 10:19:00

| Pond File:          | C:\PONDPACK\2021   | . PND |
|---------------------|--------------------|-------|
| Inflow Hydrograph:  | C:\PONDPACK\2022A2 | . HYD |
| Outflow Hydrograph: | C:\PONDPACK\OUT    | .HYD  |

## INFLOW HYDROGRAPH

## ROUTING COMPUTATIONS

|   | TIME<br>(hrs)                    | INFLOW<br>(cfs)              | I1+I2<br>(cfs)           | 2S/t - 0<br>(cfs)            | 2S/t + 0<br>(cfs)            | OUTFLOW<br>(cfs) | ELEVATION<br>(ft)            |
|---|----------------------------------|------------------------------|--------------------------|------------------------------|------------------------------|------------------|------------------------------|
| : | 0.750<br>0.767<br>0.783<br>0.800 | 0.38<br>0.26<br>0.13<br>0.00 | 0.9<br>0.6<br>0.4<br>0.1 | 27.3<br>26.0<br>24.5<br>22.9 | 29.3<br>28.0<br>26.4<br>24.7 | 0.94             | 1.34<br>1.29<br>1.24<br>1.17 |
|   |                                  |                              |                          |                              |                              |                  |                              |

C:\PONDPACK\2021 . PND Pond File: Inflow Hydrograph: C:\PONDPACK\2022A2 Outflow Hydrograph: C:\PONDPACK\OUT .HYD . HYD Starting Pond W.S. Elevation = 0.00 ft \*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\* Peak Inflow = 1.28 cfs Peak Outflow = 1.08 cfs Peak Elevation = 1.47 ft \*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\* Initial Storage 0 cu-ft = Peak Storage From Storm = 955 cu-ft \_\_\_\_\_ Total Storage in Pond = 955 cu-ft

|        | I          | POND-2 Version: 5.21 S/N:  | Page 5                                       |
|--------|------------|--|--|
|        | ]          | Pond File:C:\PONDPACK\2021Enflow Hydrograph:C:\PONDPACK\2022A2Outflow Hydrograph:C:\PONDPACK\OUT | .PND<br>.HYD<br>.HYD<br>EXECUTED: 09-30-2021 |
|        | E          | Peak Inflow=1.28 cfsPeak Outflow=1.08 cfsPeak Elevation=1.47 ft                                  | 10:19:00                                     |
|        | c          | 0.0 0.5 1.0 1.5 2.0 2.5 3.0<br>     -  | Flow (cfs)<br>3.5 4.0 4.5 5.0 5.5            |
| .05    | -          | x *<br>x *   |  |
| .07    | -          | x *<br>x *   |  |
| .09    | -          | x *<br>x *   |  |
| .1     | -          | x *<br>x *   |  |
| .12    | -          | x *<br>x *   |  |
| .14    | -          | x *<br>x *   |  |
| .15    | -          | x *<br>x *   |  |
| .17    | -          | x *<br>x *   |  |
| .19    | -          | x *<br>x *   |  |
| .2     | -          | x *<br>x *   |  |
| .22    | -          | x *<br>x *   |  |
| .24    | -          | x *<br>x *   |  |
| .26    | -          | x *<br>x *   |  |
| .27    | -          | x *<br>x *   |  |
| .29    | -          | x *<br>x *   |  |
| .31    | -          | x *<br>x *   |  |
| .32    | -          | x *<br>x *   |  |
| .34    | -          | x *<br>x *   |  |
| .36    | -          | x *<br>x *   |  |
|        | TIM<br>(hr |  |  |
| x<br>* |            | le: C:\PONDPACK\OUT .HYD Qmax =<br>le: C:\PONDPACK\2022A2 .HYD Qmax =                            |  |

Page 1 POND-2 Version: 5.21 S/N: EXECUTED: 09-30-2021 10:25:37 \*  $\mathbf{+}$  $\star$ \* OUTLET STRUCTURE FOR 682 NJ STATE HIGHWAY ROUTE 440 BLOCK 20403, LOT 1 & 2 \* \* CITY OF JERSEY CITY, HUDSON COUNTY, NJ \* \* \* \* ÷. \*\*\*\*\* Inflow Hydrograph: C:\PONDPACK\2022A10 .HYD Rating Table file: C:\PONDPACK\2021 .PND ----INITIAL CONDITIONS----Elevation = 0.00 ft 0.00 cfs Outflow = Storage = 0 cu-ft INTERMEDIATE ROUTING

GIVEN POND DATA

| ELEVATION | OUTFLOW | STORAGE |
|-----------|---------|---------|
| (ft)      | (cfs)   | (cu-ft) |
| 0.00      | 0.0     | 0       |
| 0.50      | 0.5     | 219     |
| 1.00      | 0.8     | 575     |
| 1.50      | 1.1     | 978     |
| 2.00      | 1.5     | 1,361   |
| 2.50      | 1.8     | 1,722   |
| 3.00      | 2.0     | 1,956   |

## COMPUTATIONS

| 2S/t  | 2S/t + 0 |
|-------|----------|
| (cfs) | (cfs)    |
| 0.0   | 0.0      |
| 7.3   | 7.8      |
| 19.2  | 20.0     |
| 32.6  | 33.7     |
| 45.4  | 46.9     |
| 57.4  | 59.2     |
| 65.2  | 67.2     |

Time increment (t) = 0.017 hrs.

## POND-2 Version: 5.21 S/N: EXECUTED: 09-30-2021 10:25:37

| Pond File:          | C:\PONDPACK\2021    | . PND |
|---------------------|---------------------|-------|
| Inflow Hydrograph:  | C:\PONDPACK\2022A10 | . HYD |
| Outflow Hydrograph: | C:\PONDPACK\OUT     | .HYD  |

INFLOW HYDROGRAPH

## ROUTING COMPUTATIONS

| TIME<br>(hrs) | INFLOW<br>(cfs) | I1+I2<br>(cfs) | 2S/t - 0<br>(cfs) | 2S/t + 0<br>(cfs) | OUTFLOW<br>(cfs) | ELEVATION<br>(ft) |
|---------------|-----------------|----------------|-------------------|-------------------|------------------|-------------------|
| 0.000         | 0.00            |                | 0.0               | 0.0               | 0.00             | 0.00              |
| 0.017         | 0.24            | 0.2            | 0.2               | 0.2               | 0.02             | 0.02              |
| 0.033         | 0.49            | 0.7            | 0.8               | 0.9               | 0.06             | 0.06              |
| 0.050         | 0.73            | 1.2            | 1.8               | 2.0               | 0.13             | 0.13              |
| 0.067         | 0.98            | 1.7            | 3.0               | 3.5               | 0.22             | 0.22              |
| 0.083         | 1.22            | 2.2            | 4.6               | 5.2               | 0.34             | 0.34              |
| 0.100         | 1.47            | 2.7            | 6.3               | 7.3               | 0.47             | 0.47              |
| 0.117         | 1.71            | 3.2            | 8.4               | 9.5               | 0.54             | 0.57              |
| 0.133         | 1.95            | 3.7            | 10.9              | 12.1              | 0.61             | 0.68              |
| 0.150         | 2.20            | 4.2            | 13.7              | 15.0              | 0.68             | 0.80              |
| 0.167         | 2.44            | 4.6            | 16.8              | 18.3              | 0.76             | 0.93              |
| 0.183         | 2.44            | 4.9            | 20.0              | 21.7              | 0.84             | 1.06              |
| 0.200         | 2.44            | 4.9            | 23.1              | 24.9              | 0.91             | 1.18              |
| 0.217         | 2.44            | 4.9            | 26.0              | 27.9              | 0.97             | 1.29              |
| 0.233         | 2.44            | 4.9            | 28.8              | 30.9              | 1.04             | 1.40              |
| 0.250         | 2.44            | 4.9            | 31.5              | 33.7              | 1.10             | 1.50              |
| 0.267         | 2.44            | 4.9            | 34.0              | 36.4              | 1.18             | 1.60              |
| 0.283         | 2.44            | 4.9            | 36.4              | 38.9              | 1.26             | 1.70              |
| 0.300         | 2.44            | 4.9            | 38.6              | 41.2              | 1.33             | 1.79              |
| 0.317         | 2.44            | 4.9            | 40.7              | 43.5              | 1.40             | 1.87              |
| 0.333         | 2.44            | 4.9            | 42.6              | 45.5              | 1.46             | 1.95              |
| 0.350         | 2.44            | 4.9            | 44.5              | 47.5              | 1.52             | 2.03              |
| 0.367         | 2.20            | 4.6            | 46.0              | 49.1              | 1.56             | 2.09              |
| 0.383         | 1.95            | 4.2            | 47.0              | 50.2              | 1.58             | 2.13              |
| 0.400         | 1.71            | 3.7            | 47.5              | 50.7              | 1.59             | 2.15              |
| 0.417         | 1.47            | 3.2            | 47.5              | 50.6              | 1.59             | 2.15              |
| 0.433         | 1.22            | 2.7            | 47.0              | 50.2              | 1.58             | 2.13              |
| 0.450         | 0.98            | 2.2            | 46.1              | 49.2              | 1.56             | 2.09              |
| 0.467         | 0.73            | 1.7            | 44.7              | 47.8              | 1.52             | 2.04              |
| 0.483         | 0.49            | 1.2            | 43.0              | 46.0              | 1.47             | 1.97              |
| 0.500         | 0.24            | 0.7            | 40.9              | 43.7              | 1.41             | 1.88              |
| 0.517         | 0.00            | 0.2            | 38.5              | 41.2              | 1.33             | 1.78              |

POND-2 Version: 5.21 S/N: EXECUTED: 09-30-2021 10:25:37

> Pond File: C:\PONDPACK\2021 . PND Inflow Hydrograph: C:\PONDPACK\2022A10 .HYD Outflow Hydrograph: C:\PONDPACK\OUT .HYD Starting Pond W.S. Elevation = 0.00 ft \*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\* Peak Inflow 2.44 cfs Ξ 1.59 cfs Peak Outflow = Peak Elevation = 2.15 ft \*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\* Initial Storage 0 cu-ft = Peak Storage From Storm = 1,472 cu-ft \_\_\_\_\_ Total Storage in Pond = 1,472 cu-ft

|        | I              | POND-2 Version: 5.21 S/N:  |                   | Page 4                           |
|--------|----------------|--|-------------------|----------------------------------|
|        | )<br>C<br>H    | Inflow Hydrograph: C:\PONDPACK\2022A10 .H                                | PND<br>IYD<br>IYD | EXECUTED: 09-30-2021<br>10:25:37 |
|        | c              | 0.0 0.5 1.0 1.5 2.0 2.5 3.0  | 3.5               | Flow (cfs)<br>4.0 4.5 5.0 5.5    |
| .05    | -              | x *  |                   |                                  |
| .07    | -              | x *<br>x *   |                   |                                  |
| .09    | -              | x *<br>x *   |                   |                                  |
| .1     | -              | x *<br>x *<br>x *  |                   |                                  |
| .12    | -              | x *  |                   |                                  |
| .14    | -              | x *<br>x *<br>x *  |                   |                                  |
| .15    | -              | x *  |                   |                                  |
| .17    | -              | x *  |                   |                                  |
| .19    | -              | x *  |                   |                                  |
| .2     | -              | x *  |                   |                                  |
| .22    | -              | x *  |                   |                                  |
| .24    | -              | x *  |                   |                                  |
| .26    | -              | x *  |                   |                                  |
| .27    | -              | x *  |                   |                                  |
| .29    | -              |  |                   |                                  |
| .31    | -              | x *  |                   |                                  |
| .32    | -              | x *<br>x *   |                   |                                  |
| .34    | -              | x *<br>x *   |                   |                                  |
| .36    | -              | x *<br>x *<br>x *  |                   |                                  |
|        | <br>TIM<br>(hr |  |                   |                                  |
| x<br>* |                | ile: C:\PONDPACK\OUT .HYD Qmax =<br>ile: C:\PONDPACK\2022A10 .HYD Qmax = | 1.6<br>2.4        |                                  |

Page 1 POND-2 Version: 5.21 S/N: EXECUTED: 09-30-2021 10:22:57 str. ÷ \* OUTLET STRUCTURE FOR 682 NJ STATE HIGHWAY ROUTE 440  $\mathbf{x}$ \* BLOCK 20403, LOT 1 & 2 ÷ CITY OF JERSEY CITY, HUDSON COUNTY, NJ  $\star$ \* \* + Inflow Hydrograph: C:\PONDPACK\2022A100.HYD Rating Table file: C:\PONDPACK\2021 .PND ----INITIAL CONDITIONS----Elevation = 0.00 ft Outflow = 0.00 cfs Storage = 0 cu 0.00 cfs 0 cu-ft INTERMEDIATE ROUTING COMPUTATIONS GIVEN POND DATA \_\_\_\_\_

| ELEVATION | OUTFLOW | STORAGE |
|-----------|---------|---------|
| (ft)      | (cfs)   | (cu-ft) |
| 0.00      | 0.0     | 0       |
| 0.50      | 0.5     | 219     |
| 1.00      | 0.8     | 575     |
| 1.50      | 1.1     | 978     |
| 2.00      | 1.5     | 1,361   |
| 2.50      | 1.8     | 1,722   |
| 3.00      | 2.0     | 1,956   |

| 2S/t  | 2S/t + 0 |
|-------|----------|
| (cfs) | (cfs)    |
| 0.0   | 0.0      |
| 7.3   | 7.8      |
| 19.2  | 20.0     |
| 32.6  | 33.7     |
| 45.4  | 46.9     |
| 57.4  | 59.2     |
| 65.2  | 67.2     |

Time increment (t) = 0.017 hrs.

## POND-2 Version: 5.21 S/N: EXECUTED: 09-30-2021 10:22:57

| Pond File:          | C:\PONDPACK\2021 .PND    |
|---------------------|--------------------------|
| Inflow Hydrograph:  | C:\PONDPACK\2022A100.HYD |
| Outflow Hydrograph: | C:\PONDPACK\OUT .HYD     |

INFLOW HYDROGRAPH

## ROUTING COMPUTATIONS

| TIME  | INFLOW | I1+I2 | 2S/t - 0 | 2S/t + 0 | OUTFLOW | ELEVATION |
|-------|--------|-------|----------|----------|---------|-----------|
| (hrs) | (cfs)  | (cfs) | (cfs)    | (cfs)    | (cfs)   | (ft)      |
|       |        |       |          |          |         |           |
| 0.000 | 0.00   |       | 0.0      | 0.0      | 0.00    | 0.00      |
| 0.017 | 0.34   | 0.3   | 0.3      | 0.3      | 0.02    | 0.02      |
| 0.033 | 0.68   | 1.0   | 1.1      | 1.3      | 0.08    | 0.08      |
| 0.050 | 1.02   | 1.7   | 2.5      | 2.8      | 0.18    | 0.18      |
| 0.067 | 1.36   | 2.4   | 4.2      | 4.9      | 0.31    | 0.31      |
| 0.083 | 1.70   | 3.1   | 6.4      | 7.3      | 0.47    | 0.47      |
| 0.100 | 2.04   | 3.7   | 9.0      | 10.1     | 0.56    | 0.59      |
| 0.117 | 2.39   | 4.4   | 12.1     | 13.4     | 0.64    | 0.73      |
| 0.133 | 2.73   | 5.1   | 15.8     | 17.3     | 0.73    | 0.89      |
| 0.150 | 3.07   | 5.8   | 19.9     | 21.6     | 0.84    | 1.06      |
| 0.167 | 3.41   | 6.5   | 24.5     | 26.4     | 0.94    | 1.23      |
| 0.183 | 3.41   | 6.8   | 29.2     | 31.3     | 1.05    | 1.41      |
| 0.200 | 3.41   | 6.8   | 33.7     | 36.1     | 1.17    | 1.59      |
| 0.217 | 3.41   | 6.8   | 37.9     | 40.5     | 1.31    | 1.76      |
| 0.233 | 3.41   | 6.8   | 41.9     | 44.7     | 1.44    | 1.92      |
| 0.250 | 3.41   | 6.8   | 45.6     | 48.7     | 1.54    | 2.07      |
| 0.267 | 3.41   | 6.8   | 49.2     | 52.4     | 1.64    | 2.23      |
| 0.283 | 3.41   | 6.8   | 52.5     | 56.0     | 1.72    | 2.37      |
| 0.300 | 3.41   | 6.8   | 55.7     | 59.3     | 1.80    | 2.51      |
| 0.317 | 3.07   | 6.5   | 58.5     | 62.2     | 1.88    | 2.69      |
| 0.333 | 2.73   | 5.8   | 60.4     | 64.3     | 1.93    | 2.82      |
| 0.350 | 2.39   | 5.1   | 61.6     | 65.5     | 1.96    | 2.90      |
| 0.367 | 2.04   | 4.4   | 62.1     | 66.0     | 1.97    | 2.93      |
| 0.383 | 1.70   | 3.7   | 61.9     | 65.8     | 1.97    | 2.92      |
| 0.400 | 1.36   | 3.1   | 61.1     | 65.0     | 1.94    | 2.86      |
| 0.417 | 1.02   | 2.4   | 59.6     | 63.5     | 1.91    | 2.77      |
| 0.433 | 0.68   | 1.7   | 57.6     | 61.3     | 1.85    | 2.64      |
| 0.450 | 0.34   | 1.0   | 55.1     | 58.7     | 1.79    | 2.48      |
| 0.467 | 0.00   | 0.3   | 52.0     | 55.4     | 1.71    | 2.35      |
|       |        |       |          |          |         |           |

|        | PO               | OND-2 Version: 5.21 S/N:   | Page 4                        |
|--------|------------------|--|-------------------------------|
|        | In               | ond File: C:\PONDPACK\2021 .PND<br>nflow Hydrograph: C:\PONDPACK\2022A100.HYD<br>ntflow Hydrograph: C:\PONDPACK\OUT .HYD | EXECUTED: 09-30-2021          |
|        | Pe               | eak Inflow = 3.41 cfs<br>eak Outflow = 1.97 cfs<br>eak Elevation = 2.93 ft   | 10:22:57                      |
|        | 0.               | .0 0.5 1.0 1.5 2.0 2.5 3.0 3.5 4   | Flow (cfs)<br>4.0 4.5 5.0 5.5 |
| 0.5    | i                |  | .         -                   |
| .05    | -                | x *  |                               |
| .07    | -                | x *  |                               |
| .09    | -                | x *<br>x *<br>x *  |                               |
| .12    | -                | x *<br>x *   |                               |
| .14    |                  | x *<br>x *<br>x *  |                               |
| .15    | -                | x *<br>x *   |                               |
| .17    | -                | x *<br>x *   |                               |
| .19    | -                | x *<br>x *   |                               |
| . 2    | -                | x *  |                               |
| .22    | -                | x *  |                               |
| .24    | -                | x *  |                               |
| .26    | -                | x *  |                               |
| .27    | -                | x *  |                               |
| .29    | -                | x *  |                               |
| .31    | -                | x *  |                               |
| .32    | -                | x *  |                               |
| .34    | -                | x *  |                               |
| .36    | -                | x *<br>x *<br>x*   |                               |
|        | <br>TIME<br>(hrs |  |                               |
| x<br>* | Fil<br>Fil       |  |                               |



## **Conclusion**

The proposed ADS pipe storage is sufficient to convey a 2- year storm by using the modified rational method. Therefore, we comply with N.J.A.C. 7:8- Stormwater Management Standards. Additionally, the following table shows the reduction for 2, 10, and 100 years' storm analyses.

| C1          | EXISTING<br>(CFS)<br>C2 | REDUCTION<br>(CFS)<br>C3 | UN-DETAINED<br>(CFS)<br>C4 | ROUTING<br>(CFS)<br>C5 | ALLOWABLE<br>(CFS)<br>(C3-C4)<br>C6 | STORAGE<br>(CU.FT.)<br>C7 |
|-------------|-------------------------|--------------------------|----------------------------|------------------------|-------------------------------------|---------------------------|
| 2 YEAR      | 2.56                    | 50% = 1.28               | 0.10                       | 1.08                   | 1.18                                | 1,223                     |
| 10<br>YEAR  | 3.39                    | 75% = 2.54               | 0.13                       | 1.59                   | 2.41                                | 836                       |
| 100<br>YEAR | 4.42                    | 80% = 3.54               | 0.16                       | 1.97                   | 3.38                                | 842                       |



| GENERAL INSPECTION, MAINTENANCE & CLEANING PROCEDURES |   |   |   |  |           |  |  |  |
|---|---|---|---|--|-----------|--|--|--|
| F   | FOR INLETS, MANHOLES, PIPES & DETENTION SYSTEM  |   |   |  |           |  |  |  |
| 2.<br>3.<br>4.<br>5.<br>6.<br>7.                      | REMOVE GRATI<br>SKIM OFF OILS<br>USING A STAD<br>IF SEDIMENT IS<br>IF NOT PROCE<br>VACUUM OR M<br>REPLACE GRA | E OR COVER.<br>S AND FLOATAI<br>DIA ROD, MEASI<br>S AT A DEPTH<br>ED TO STEP 7<br>IANUALLY REM<br>TE. | BLES.<br>URE THE DEF<br>GREATER TH<br>OVE SEDIMEN | TENTION SYSTEM FOR SEDIMENT ANNU<br>PTH OF SEDIMENT.<br>IAN 6" PROCEED TO STEP 6.<br>IT.<br>E NEXT INSPECTION. | ALLY.     |  |  |  |
|   |   |   | SEDIMENT  |  |           |  |  |  |
| DATE  | FIXED POINT TO<br>CHAMBER BOTTOM (1)  | FIXED POINT TO<br>TOP OF SEDIMENT (2)   | DEPTH<br>(1) - (2)                                | OBSERVATIONS/ACTIONS   | INSPECTOR |  |  |  |
|   |   |   |   |  |           |  |  |  |
|   |   |   |   |  |           |  |  |  |
|   |   |   |   |  |           |  |  |  |
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|   |   |   |   |  |           |  |  |  |

## **GENERAL INSPECTION, MAINTENANCE & CLEANING PROCEDURES** FOR INLETS, MANHOLES, PIPES & DETENTION SYSTEM

1. INSPECT INLETS, MANHOLES, PIPES & DETENTION SYSTEM FOR SEDIMENT ANNUALLY.

- 2. REMOVE GRATE OR COVER.
- 3. SKIM OFF OILS AND FLOATABLES.
- USING A STADIA ROD, MEASURE THE DEPTH OF SEDIMENT.
   IF SEDIMENT IS AT A DEPTH GREATER THAN 6" PROCEED TO STEP 6. IF NOT PROCEED TO STEP 7.
- 6. VACUUM OR MANUALLY REMOVE SEDIMENT.
- 7. REPLACE GRATE.
- 8. RECORD DEPTH AND DATE AND SCHEDULE NEXT INSPECTION.

| DATE | STADIA ROI                           | READINGS                              | SEDIMENT<br>DEPTH | OBSERVATIONS/ACTIONS | INSPECTOR |
|------|--------------------------------------|---------------------------------------|-------------------|----------------------|-----------|
| DATE | FIXED POINT TO<br>CHAMBER BOTTOM (1) | FIXED POINT TO<br>TOP OF SEDIMENT (2) | (1) - (2)         | Obelivation          |           |
|      |                                      |                                       |                   |                      |           |
|      |                                      |                                       |                   |                      |           |
|      |                                      |                                       |                   |                      |           |
|      |                                      |                                       |                   |                      |           |
|      |                                      |                                       |                   |                      |           |
|      |                                      |                                       |                   |                      |           |
|      |                                      |                                       |                   |                      |           |
|      |                                      |                                       |                   |                      |           |
|      |                                      |                                       |                   |                      |           |
|      |                                      |                                       |                   |                      |           |

### Sample Maintenance Log

| Date    | Stadia rod<br>Fixed point<br>to chamber<br>bottom (1) | readings<br>Fixed point<br>to top of<br>sediment (2) | Sediment<br>Depth<br>(1) - (2) | Observations/Actions  | Inspector |
|---------|---|--|--------------------------------|---|-----------|
| 3/15/01 | 6.3 ft  | none   |                                | New installation. Fixed point is CI frame at grade                            | djm       |
| 9/24/01 |   | 6.2  | 0.1 ft                         | Some grit felt  | sm        |
| 6/20/03 |   | 5.8  | 0.5 ft                         | Mucky feel, debris visible in manhole and in<br>isolator row, maintenance due | rv        |
| 7/07/03 | 6.3 ft  |  | 0                              | System jetted and vacuumed  | djm       |

## Additional Notes

1. INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION, ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS:

2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY

THE OWNER OF THE PROPERTY, MYNENI PROPERTIES, LLC. IT'S SUCCESSORS AND/OR ASSIGNS, WILL BE RESPONSIBLE FOR THE MAINTENANCE OF THE INLETS, MANHOLES, PIPES & DETENTION SYSTEM ON THE PROPERTY LOCATED AT 882 NJ STATE HIGHWAY 440 CITY OF JERSEY CITY, NJ TEL: 201-424-4409



United States Department of Agriculture

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

# Custom Soil Resource Report for Hudson County, New Jersey



## Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2\_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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| How Soil Surveys Are Made                                 | 5  |
| Soil Map  |    |
| Soil Map  |    |
| Legend  | 10 |
| Map Unit Legend   |    |
| Map Unit Descriptions                                     |    |
| Hudson County, New Jersey                                 |    |
| URTILB-Urban land, till substratum, 0 to 8 percent slopes |    |
| URWETB-Urban land, wet substratum, 0 to 8 percent slopes  |    |
| References  |    |

## **How Soil Surveys Are Made**

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

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identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

## Custom Soil Resource Report Soil Map



Custom Soil Resource Report

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| The soil surveys that comprise your AOI were mapped at 1:12,000.<br>Warning: Soil Map may not be valid at this scale.<br>Enlargement of maps beyond the scale of mapping and accuracy of soil misundenstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.<br>Flease rely on the bar scale on each map sheet for map measurements.<br>Source of Map: Natural Resources Conservation Service Web Soil Survey URL:<br>Coordinate System: Web Mercator (EPSG:3857)<br>Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area are required.<br>This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.<br>Soil Survey Area: Hudson County, New Jersey Streek from the USDA-NRCS certified data as from the version date(s) listed below.<br>Soil Survey Area are are required.<br>This product is generated from the USDA-NRCS certified data as the accurate calculations of distance or area are required.<br>This product is generated from the USDA-NRCS certified data as the soil Survey Area area: Version 10, Jun 1, 2020<br>Soil Survey Area area is the below.<br>Soil survey Area area is the space allows) for map scales 1:50,000 or larget. | Spoil Area<br>Story Spot<br>Very Story Spot<br>Wet Spot<br>Wet Spot<br>Other<br>Special Line Features<br>Streams and Canals<br>on<br>alls<br>Interstate Highways<br>Streams and Canals<br>on<br>alls<br>Major Roads<br>Other<br>Streams and Canals<br>Streams and Canals<br>on<br>Alls<br>Streams and Canals<br>Streams and Streams<br>Streams and Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams<br>Streams | β ν  | Spoil Area<br>Story Spot<br>Very Story Spot<br>Wet Spot<br>Other<br>Special Line Features<br>Streams and Canals<br>Streams and Canals<br>Streams and Canals<br>Streams and Canals<br>US Routes<br>Major Roads<br>Local Roads<br>Local Roads<br>derial Photography  |                                       |  |   | ator<br>the  | a<br>a   |   | Sep                                 |
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| Map Unit Symbol             | Map Unit Name   | Acres in AOI | Percent of AOI |
|-----------------------------|---|--------------|----------------|
| URTILB                      | Urban land, till substratum, 0 to<br>8 percent slopes | 0.9          | 98.5%          |
| URWETB                      | Urban land, wet substratum, 0 to 8 percent slopes     | 0.0          | 1.5%           |
| Totals for Area of Interest |   | 0.9          | 100.0%         |

## **Map Unit Legend**

## Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however,

onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

## **Hudson County, New Jersey**

## URTILB—Urban land, till substratum, 0 to 8 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2qjwr Elevation: 0 to 520 feet Mean annual precipitation: 30 to 56 inches Mean annual air temperature: 47 to 63 degrees F Frost-free period: 179 to 217 days Farmland classification: Not prime farmland

#### Map Unit Composition

Urban land, till substratum: 90 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

### **Description of Urban Land, Till Substratum**

#### Setting

Landform position (two-dimensional): Summit Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Asphalt over human-transported material

## **Typical profile**

*M* - 0 to 15 inches: material 2<sup>C</sup> - 15 to 79 inches: gravelly sandy loam

### **Properties and qualities**

Slope: 0 to 8 percent
Depth to restrictive feature: 0 inches to manufactured layer
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00 in/hr)
Calcium carbonate, maximum content: 10 percent
Available water capacity: Very low (about 0.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8s Hydric soil rating: Unranked

### **Minor Components**

#### Greenbelt

Percent of map unit: 10 percent Landform position (two-dimensional): Summit, backslope, footslope Landform position (three-dimensional): Crest, side slope, base slope, talf Down-slope shape: Linear, convex Across-slope shape: Linear, convex Hydric soil rating: No

## URWETB—Urban land, wet substratum, 0 to 8 percent slopes

#### **Map Unit Setting**

National map unit symbol: 13q0j Elevation: 0 to 520 feet Mean annual precipitation: 30 to 64 inches Mean annual air temperature: 46 to 79 degrees F Frost-free period: 131 to 213 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

Urban land, wet substratum: 90 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

### **Description of Urban Land, Wet Substratum**

### Setting

Landform position (two-dimensional): Summit Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Asphalt over human-transported material

#### **Typical profile**

M1 - 0 to 6 inches: material M2 - 6 to 20 inches: material 2<sup>C</sup>u - 20 to 79 inches: very artifactual coarse sandy loam

#### **Properties and qualities**

Slope: 0 to 8 percent Depth to restrictive feature: 0 inches to manufactured layer Runoff class: Very high Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00 in/hr) Depth to water table: About 20 inches Calcium carbonate, maximum content: 19 percent Available water capacity: Very low (about 0.0 inches)

## **Interpretive groups**

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8s Hydric soil rating: Unranked

### **Minor Components**

## Parsippany, frequently flooded

Percent of map unit: 5 percent Landform: Lake terraces Landform position (two-dimensional): Toeslope

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Landform position (three-dimensional): Dip Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

Whippany

.

Percent of map unit: 5 percent Landform: Lake terraces Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Dip Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

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